Second Monthly Progress Report

Thermal Strain Analysis

of

on

Advanced Manned-Spacecraft Heat Shields

NASA Contract NAS 9-1986 Period 19 September 1963 to 26 October 1963

> ARA Report #27

Prepared by:

Daniel H. Platus, Project Scientist

Shoichi Uchiyama, Project Scientist

Approved by:

B. Mazelsky, President, ARY, Inc.

OTS PRICE

XEROX \$ \frac{1}{\sigma}

MICROFILM \$ 0.50 mf

SECOND MONTHLY PLOGRED - NOTION THERE - SERVIN ANALYSIS OF ADVANCED MANNED-SPACECRAFT - 1 THELDS

NA . Contract NAS 9-1986

Phase A - Derivation of Basic Equations

This phase of the study, which constitutes the derivation of the basic equilibrium and stress equations in spherical and toroidal coordinates, is 95% completed.

The only portion which is not included in this report (Appendix A) consists of defining certain coefficients in the equilibrium and stress equations which become singular on the axis of symmetry in the non-axisymmetric case. The singular point can be evolided in the numerical evaluation of the problem. However, if the number of grid nodes is limited by machine storage such that omission of the axis of symmetry would result in appreciable error in the remaining nodes, it is important to include this point. An analytical method has been developed for treating the singularity and it is anticipated that all of the necessary coefficients for the numerical evaluation with a obtained within one week

Phose B - Finite Difference Formula:

All of the finite or along now a particulative difference of the grant and a contract of the particular of the particular of the particular of the phase.

The same congress of the particular of the phase.

Library Copy

SEP 1934

Manned Spacecraft

Center

Houston, Texas

equations using the finite difference analogs. Since these coefficients will be generated with the aid of the IBM 7090, the work will require close coordination between the Project Scientist and Programmer and will be carried out as a joint effort.

Phase G - Report Preparation

This second monthly progress report constitutes 5% of the total report writing phase, which brings the total effort expended in this phase to 8%. In the next report (First Quarterly Progress Report), all of the work to date will be summarized in a complete, comprehensive report.

APPENDIX A (Continued)

Derivation of Equilibrium and Stress Equations
in Terms of Displacements in Spherical and Toroidal
Coordinates

Construction of Finite Difference Analogs to
Differential Equations

Summary

The work contained herein is a continuation of Appendix A presented in the First Monthly Progress Report, NASA Contract NAS 9-1986. Page numbers, figure numbers, table numbers and equation numbers are continued in consecutive order and reference is made to equations in the first progress report without repetition of the equations in this report. It should be noted that Fig. 1 refers to the two coordinate systems on the first page of Appendix A and Tables I and 2 refer to the coefficients of the equilibrium equations in spherical and toroidal coordinates, respectively, which were not labeled in the first report.

```
Equations for Stresses in Trime of Displacements
From Hooke's law, Eqs. (9) and (10) s
                                                                                  (17)
    T_{ij} = 2\mu e_{ij} + \delta_{ij} \left[ \lambda \phi - (3\lambda + 2\mu \epsilon) \int_{T} \kappa(T) dT \right]
   where Sij is the Kronecker delta defined by
             \delta y = 1, \quad i = j
= 0, \quad i \neq j
             Q = 4, + 22 + 233.
     Writing the strains in terms of displacements from either

Egs. (14) or (15) and shortening The nomenclature by defining

The stresses
      The Stresses
                       7, = Trr or TRR
                     72 = 704
                       73 = 700
                       Ty = Try or Try
                       75 = Tpo
```

 $T_6 = T_{ro}$ or T_{RO} $E_{g.(17)}$. may be written in Terms of displacements according T_{ro}

Where
$$\Delta l = 1$$
 if $l = 1, 2, 3$
= 0 if $l = 4, 5, 6$

Equations at the Avis of Summetry

Certain of the coefficients in the displacement Equilibrium, and stress again become singular at the axis of symmetry (9=0). For the non-axially-symmetric case the axis of symmetry has no special physical significance and this point can be avoided. For the axially-symmetric case, however, the axis of symmetry is generally quite important and the singular coefficients may be evaluated by the use of L'Hôpitals rule. For example, the coefficient H, in the displacement equilibrium equations in spherical coordinates is μ cate/ R^2 which becomes infinite as φ approaches zero. From Eq. (16), this term multiplies the displacement component $\frac{\partial u}{\partial \varphi}$. The conditions for axial symmetry are

 $W(R, P, 0) = \frac{2}{50} = 0$, (19)

from which it can be shown that $v = \frac{\partial u}{\partial \varphi} = \frac{\partial v}{\partial \varphi^2} \quad \text{at } \varphi = 0 . \tag{20}$

Hence, since du approaches zero While H, approaches infinity, L'Hôpital's rule is applicable to the product

Mater du

as $\varphi \to 0$. Taking the limit, there is obtained $\lim_{\varphi \to 0} \frac{\mu \cot \varphi}{R^2} \frac{\partial u}{\partial \varphi} = \frac{\mu}{R^2} \lim_{\varphi \to 0} \frac{\frac{\partial u}{\partial \varphi} \cos \varphi}{\sin \varphi}$ $= \frac{\mu}{R^2} \lim_{\varphi \to 0} \frac{\frac{\partial u}{\partial \varphi} \cos \varphi}{\cos \varphi} = \frac{2u}{2\varphi} \sin \varphi$

 $= \frac{\mu}{R^2} \cdot \frac{\partial^2 u}{\partial \varphi^2}$

Hence, for this case, the coefficient H, becomes zero and The coefficient B, which multiplies du is increased by M/R. Applying this limiting process to all the singular terms the following this coefficients are obtained:

Taste 4

coefficients of Equilibrium Equations on Axis of Symmetry (\$\phi = 0\$) for Axially-Symmetric Case Sperical Coordinates

L	/	20	3 (4)	R	/	20	3 [©]	£	, 0	20	30
Az	2+2/4 B	0	C	À	0 0	0	O	Āĸ	0	0	0
B	24/20		0	Ē	0 0	0	0	ĒŁ	0	0	0
Ca	OD		0	CA	0 0	0	0	Ē,	0	0	0
De	00	0	Ó	Dx	2(X+M)/R®	0	0	Da	0	0	0
E	00	0	0	Ē	0	0	O	EA	O	0	0
FR	00	0	0	FX	0	0	O	FX	O	0	0
Ge	2 (X+2 M)/RO	Ö	0	G	00	ن	0	GR	0	0	0
HA	0 0	O	0	FIR	$-2(\lambda+3\mu)/R^2$	0	0	HA	0	0	0
Ix	0 9	0	0	I	0 0	0	0	7	0	0	0
J		<u> </u>	0	J,	0	0	0	7	0	0	0

Table 5

Coefficients of Stress Equations on Axis of Symmetry (\$\phi = 0\$) for Axially - Symmetric Case Spherical Coordinates

	- 6	
וב		
	0	0
9	. 0	0
9	0	0
Ø	0	6
9	0	المت
2	· O	(2)
٧	0	0
0	0	Ø
0	H	(9)
	0	نت
6	0	0
0	- 11/R	(i)
	000000000000000000000000000000000000000	

If, in addition to the coefficient of Thermal expansion, the elastic constants are strongly dependent on Temperature, then additional terms must be included in the displacement equilibrium equations to account for the spacial derivatives of these constants. Differentiating the stress component The with respect to coordinate di, for example, from Eq. (9), There is obtained

$$\frac{\partial T_{ii}}{\partial u_{i}} = \lambda \frac{\partial \Phi}{\partial u_{i}} + \Phi \frac{\partial \lambda}{\partial u_{i}} + 2\mu \frac{\partial e_{ii}}{\partial u_{i}} + 2e_{ii} \frac{\partial \mu}{\partial u_{i}}$$

$$= -(3\lambda + 2\mu) \omega(\tau) \frac{\partial T}{\partial u_{i}} \oplus \frac{\partial}{\partial u_{i}} (3\lambda + 2\mu) / \omega(\tau) d\tau$$

$$= \Phi \frac{\partial \lambda}{\partial \tau} \frac{\partial T}{\partial u_{i}} + 2e_{ii} \frac{\partial \mu}{\partial \tau} \frac{\partial T}{\partial u_{i}} \oplus \frac{\partial}{\partial \tau} (3\lambda + 2\mu) \frac{\partial T}{\partial u_{i}} / \omega(\tau) d\tau$$

$$+ \lambda \frac{\partial \Phi}{\partial u_{i}} + 2\mu \frac{\partial e_{ii}}{\partial v_{i}} - (3\lambda + 2\mu) \omega(\tau) \frac{\partial T}{\partial u_{i}}$$

$$= (21)$$

where the first three terms to the right of the equal sign have not been accounted for in the coefficients of Eq. (16). Representing the additional terms by primed quantities, Eq. (16) becomes

(AR+AR)
$$\frac{\partial u}{\partial u^2} + (BR+BR) \frac{\partial u}{\partial u^2} + \cdots = \frac{(3\lambda+2\mu) \times (\tau)}{\sqrt{94\pi}} \frac{\partial \tau}{\partial u}$$

4

The coefficients AR, BR, ... are taisulated below for spherical and toroidal coordinates, and for the special point in Spherical coordinates on The axis of Symmetry for The case of axial symmetry.

1. Sur

	The state of the s	. (المترسمات	Condinates	5	0 - 2	
			7 34 2		£=3	0
	78 = 1	And the second s	0	(4)	0	0
6	0	سنت عديد في والاستادات	0	6	0	0
. T	0	<u>い</u>	and the confidence of the conf	0	0	0
2	0	0	0	0	0	1
é .	Company of the same of the sam	9	<u> </u>		0	0
2		(w)	0	0	0	9
Ž.	0	O	0			0
1	0		1 2X 2T	0 1	train of 27 20	
· · · - · I	류(2+24) 하	9	$\frac{1}{r}\frac{\partial \lambda}{\partial \tau}\frac{\partial T}{\partial \varphi}$	0	and the second s	0
GZ		0	1 du dr r ar ar		0	
	一 学 30		r ar ar	0 -	1 du dr	0
HR	70 01	ST O	0		+rain of or	MILE
I'A	(a+rain q) = 27	56	and the second of the second o	3,97	1+ rain \$ 37 2+ rain \$ 27 (2+24) \$7 +	187 39 (Any day d)
4	$\frac{1}{r} + \frac{\sin \varphi}{a + r \sin \varphi} \bigg) \frac{\partial}{\partial \varphi}$	X STO 1	= = (\(\lambda + 2\mu \) \frac{\partial T}{2\pi} + \frac{\partial m}{(a+r)} \frac{\partial T}{2\pi} + \frac{\partial m}{(a+r)} \frac{\partial T}{2\pi}		2+roine) = 31 (100)	6
J. (++ a+rainq) ?	For r		0	0	
	0	0	The second secon	0	0	0
ĀŁ	0	0		0	• 6	9
BA	and a company of the control of the	0	6	0	0	0
CA	<u> </u>	G)	0	1_	0 %	6
	0	0	C .	0	The state of the s	ا
Đạ Ēi	0	0	0	0	0	0
Fi	0		Ju at	0		
	一种	9	紫芷)3 3:	r Ø
Gi	r 37 39	- 0	1 3 /2+2/1 2		r(a+raing) 27 20	<u> </u>
	广兴	I C	1- 3- (A+24) 3-	(2.46	TU
FLE	r 37 3	0	(a+ rain q) = 2 de 27 26	_ 0		4
=1	0	J	(a+ rain 4) 2 3T 26	د. استار استان	(a+raing) = ot (n+	24) 3T (
$\bar{\mathcal{I}}_{\mathcal{K}}$	33 37	131.376	and didi	十类架	(a+raine) or ("	* Year a management
J'	a+rsing or or	市斧師	r(a+rsing) 27 34	·		
L .~-h	a+1 mm 4	9	0		0	U
Āk		0	0		The second section is not a second se	E
BA	0		0		The second second second second second second second second second	G
CÉ	0			Č.	The second section of the second section is a second section of the second section of the second section section section sections and the second section secti	<u></u>
	0		Committee of the Commit	· (e		
2	0		The second secon	(ر. در دوسوس دورورسوشهٔ وس
EX	0		9		9 34 3T	. (
FA	July du	DT (9			
DA EX FA	1 a+rain 9 37	= 37	Ju à	-	中部	ē
		and the control of th	r(a+rsin 4) ot o	7	1 - 01	· dT
Ä	4	and the second s	(at 1))	(a+raina) 2 \$7()	1+24) 27
		$=\frac{\partial T}{\partial r}$	rations) of	the same and the same of the s		- 1 JT -
\ 1			(a. ram \$) = 37	L OT	- 34 Same (St. Din	中土一
1	$\frac{1}{\sqrt{1+\frac{\sin \varphi}{(a+r\sin \varphi)^2}}}$	DIL OT	- 2 37	- 26	0.4-1/	

V.

Additional Terms in Coefficients of Problemium Exportants
from Temperature & sentince of Elastic Constants
Spherical Coordinates

Г	£=/		p = 2		k = 3	
12	X= /	6	The state of the s	0	e internationale appearant de compressionale destaurant de compression de la proposition de la compression della compres	79
AR	Annual Annual and the second and the	0	0	0	0	0
Be		9		9		<u></u>
CE	0	i	<u> </u>		0	
DR		9	The properties of the properties of the contract of the contra	0		6
EX		9	The second of th	0		0
FR	0	9	Ű	Ð	0	0
GA	∂ 5+ (λ+2μ) ∂T 8R	9	TR OT OP	0	Raine or de	0
HÉ	力がず	0	× 34 37 3R	Ø	0	©
I'	Rain of 26	0	0	0	Paint of TR	0
J2.	差异蓝	0	2 3 (h+ 1) 3T	0	Rzing 27 (2+41)	TO 38
ĀŔ	0	9	0	0	0	0
	. 0	0	0	0		0
B'z Ĉź	0	8		0	0	0
De	0	Se l		0		0
ĒŔ	0	اعلى	0	6	. 0	0
R		9		0	0	0
Ē,	र्र रेम रेम	0	34 3T 37 3R	9		0
H'A	大部分	0	χ 2 2 (λ+2μ) 27 χ 2 2 (λ+2μ) 27	9	Raine IT 30	0
$\bar{\mathcal{I}}_{\mathbf{z}}'$	0	0	Rainia de 27	٧	Rung of Sp	9
完'	32 37 coto - k2 34 37 28 27	JT ₩ 34	Cot 9 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 pm	$\frac{\cot \varphi}{R^2 \sin \varphi} \frac{\partial}{\partial T} (\lambda + 2\mu)$	276
Āź	0	انف	0	0	0	\mathcal{Q}
Āź Bź	promote and the second	9	O	0	0	رسی
Čá	0	9	0	0	0	(D)
Die	0	3	O (9	0	(چي
7	0	<u>(j)</u>	O	0	O	10
EK FR	0	(9)	0	0	G	(2)
Ĝ's	Rain & DT DO	9	0	0	DE DE	(Q) (Q) (Q)
FI'A	0	<i>₩</i>	Raing of DE	٩	1 du de	9
式	Roma of DR	9	Rainy of de		R2sin & d (2+2+2) dt	٨
灵	- I du dT	9	- Cot of de de de - Raing of do		一点给你一块里	

Axis of Symmetry with Aximi symmetry

The only non-zero terms in the coefficients of

Table 6 on the axis of symmetry in the axially
symmetric case are The following:

The integral term in Eq. (22) is also non-zero for the equilibrium equation corresponding to k=1.

Finite Difference Formulation

The difference analogs to The partial differential equations are constructed on a grid network as shown in Fig. 2, for which & = constant lines are ordered by The subscript i, & = constant lines by The subscript j d3 = constant lines by the subscript k, and the intersection of grid lines (nodes) by The triple subscript i, j, k.

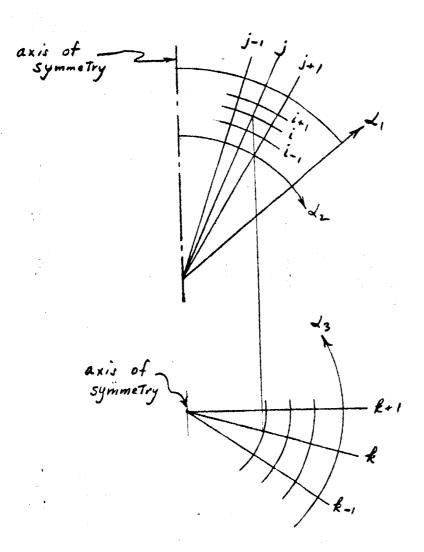


Fig 2 Grid Notation for Finite Difference FormulaTion

For the general case the grid spacing will be irregular and the increments in the vicinity of a mode will be designated by the following:

$$h_{11} = (d_1)_{i+1} - (d_1)_i \qquad h_{21} = (d_2)_{i+1} - (d_2)_i \qquad h_{21} = (d_2)_{i+1} - (d_2)_i$$

$$h_{12} = (d_1)_{i+2} - (d_1)_i \qquad h_{22} = (d_2)_{i+2} - (d_2)_i \qquad h_{21} = (d_2)_{i+2} - (d_3)_i$$

$$h_{13} = (d_1)_i - (d_1)_{i-1} \qquad h_{23} = (d_2)_i - (d_2)_{i-1} \qquad h_{33} = (d_3)_i - (d_3)_{i-1}$$

$$h_{14} = (d_1)_i - (d_1)_{i-2} \qquad h_{24} = (d_2)_i - (d_2)_{i-2} \qquad h_{34} = (d_3)_i - (d_3)_{i-2}$$

Let $f(x_1,d_2,d_3)$ be any function of the Coordinates such that it and its partial derivatives (up to any order required in the analysis) are continuous, and expand the function about the point i,j,k. Using a new coordinate system with origin at i,j,k and with 51,52,53 directed along k,k2,k3, respectively, the function f(51,52,53) is written

$$f(s_1, s_2, s_3) = f'_{i,j}, k + B, s_1 + B_2 s_2 + B_3 s_3 + B_4 s_1 s_2 + B_4 s_3 + B_6 s_2 + B_4 s_3 + B_6 s_3 s_1 + B_7 s_1^2 + B_8 s_2^2 + B_4 s_3 + B_{12} s_1^2 s_2^2 + B_{12} s_1^2 s_3^2 +$$

The first and second derivatives of $f(x_1, x_2, x_3)$ with respect to $\alpha_1, \alpha_2, \alpha_3$ are obtained from Eq. (23) according to $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (23) according to $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$ and $\frac{\partial f}{\partial x_2}$ are obtained from Eq. (24) $\frac{\partial f}{\partial x_1}$

By considering the values of f(\$1, \$:, \$3) at the twelve nodes adjacent to i,j, &, the constants Bi are evaluated in terms of the function at there modes and The grid spacings as shown in Fig. 3.

The grid spacings as show	an rei 7 g · u	Node	. Coordinate
2	£, (d2)	0	(i,j,t) (i+1,j,t) (i+2,j,t)
h ₂₄	10	3	(i-1, j, *) (i-2, j, k)
8 has had 9	haz	5 6	(6, j+1, 4) (6, j+2, 4) (6, j+1, 4)
hat 11 3 has	5 (4)	8 9	(6, 1, 2+4)
hw har	1	10 11 12	(i,j, k+2) (i,j, k-1) (i,j, k-2)
4	72.		
	Lucia Mach In	tervals	

Eig. 3 Coordinates of Irregular Mesh Intervals

Note that the grid spacing increments his do not, in general, have the dimensions of length but have the dimensions of di, dr and dr.

At points 1 and 3, Eq. (23) becomes

At points 1 and 3, Eq. (23) becomes

$$\begin{cases} f(h_{ij}, o, o) = f(ij, k + \beta, h_{ij} + \beta, h_{ij}) \\ f(i), j, k = f(-h_{ij}, o, o) = f(ij, k - \beta, h_{ij}) + \beta, h_{ij} \end{cases}$$

(25)

where terms of higher order are deleted. Solving for where terms of higher order for The first and Second

. B, and By from Eqs. (25) gives for The first and second irregular central derivative with respect to 4,

Substituting to his = his into Egs. (26) gives for the second regular central derivatives with first and respect to

$$\frac{\partial f}{\partial d_{i}}\Big|_{i,j,k} = \frac{f_{i+1,j,k} - f_{i-1,j,k}}{2h_{i}}$$

$$\frac{\partial^{2} f}{\partial d_{i}}\Big|_{i,j,k} = \frac{f_{i+1,j,k} - 2f_{i,j,k} + f_{i-1,j,k}}{h_{i}^{2}}$$
(27)

By a similar procedure The following first and second regular and Irregular contral derivatives are obtained with respect to the coordinates & and & :

First Regular Central Derivatives
$$(h_2 = h_{21} = h_{22}, h_3 = h_{23})$$

$$\frac{\partial f}{\partial u_2}|_{i,j,k} = \frac{f_{i,j+1,k} - f_{i,j-1,k}}{2h_2}$$
(28)

$$\frac{2f}{2d_3}\Big)_{i,j,k} = \frac{f_{i,j,k+1} - f_{i,j,k-1}}{2h_3} \tag{29}$$

First Invegular Central Derivatives

$$\frac{\partial f}{\partial d_{2}}\Big|_{i,j,k} = \frac{h_{23}^{2} f_{i,j+1,k} + (h_{2i}^{2} - h_{23}^{2}) f_{i,j,k} - h_{2i} f_{i,j-1,k}}{h_{2i} h_{23} (h_{2i} + h_{23})}$$
(20)

$$\frac{2f}{\partial d_3}|_{i,j,k} = \frac{h_{33} f_{i,j,k+1} + (h_{31} - h_{32}) f_{i,j,k} - h_{31} f_{i,j,k-1}}{h_{31} h_{33} (h_{31} + h_{32})}$$
(31)

Second Regular Central Derivatives
$$(h_2 = h_{21} = h_{22}, h_3 = h_{31} = h_{33})$$

$$\frac{3+}{3d_2}\Big|_{i,j,k} = \frac{f_{i,j+1,k} - 2f_{i,j,k} + f_{i,j-1,k}}{h_2}$$

$$\frac{3+}{3d_2}\Big|_{i,j,k} = \frac{f_{i,j+1,k} - 2f_{i,j,k} + f_{i,j-1,k}}{h_2}$$
(32)

$$\frac{\partial f}{\partial k_{s}^{*}}\Big)_{i,j,k} = \frac{f_{i,j,k+1} - 2f_{i,j,k} + f_{i,j,k-1}}{h_{s}^{*}}$$

Second Presquier Control Devivations

$$\frac{\partial \tilde{T}}{\partial d_{2}^{2}}\Big|_{i,j,k} = \frac{2[h_{23}f_{i,j+1,k} - (h_{2i} + h_{2i})f_{i,j,k} + h_{2i}f_{i,j-1,k}]}{h_{2i}h_{23}(h_{2i} + h_{23})}$$
(34)

$$\frac{3\frac{2}{f}}{3d_{5}^{2}}\Big|_{i,j,k} = \frac{2\left[h_{23}f_{i,j,k+1} - (h_{31} + h_{33})f_{i,j,k} + h_{31}f_{i,j,k-1}\right]}{h_{31}h_{23}(h_{31} + h_{33})}$$
(35)

Forward and Backward Derivatives

By applying the same procedure as above with respect to Two nodes located either forward or bockward from The origin (ij, k), The first and second regular and irregular derivatives are obtained in terms of the function f(d,, d,, d) evaluated at these modes. The results are summarized below for the three coordinate directions

$$\frac{First\ /regular\ Forward\ Derivativas}{\frac{2f}{\partial k_{1}}}\Big|_{i,j,k} = \frac{-\left(h_{i2}^{2} - h_{i1}^{2}\right)f_{i,j,k} + h_{i2}f_{i+1,j,k} - h_{ii}f_{i+2,j,k}}{h_{ii}h_{i2}\left(h_{i2} - h_{ii}\right)}$$

$$(36)$$

$$\frac{2f}{\partial d_{\perp}}\Big)_{i,j,k} = \frac{-\left(h_{22}^{2} - h_{21}^{2}\right)f_{i,j,k} + h_{22}f_{i,j+1,k} - h_{21}f_{i,j+2,k}}{h_{21}h_{22}\left(h_{22} - h_{21}\right)} \tag{37}$$

$$\frac{\partial f}{\partial t_3}\Big|_{ij;k} = \frac{-\left(h_{32} - h_{31}^2\right) f_{i,j,k} + h_{32} f_{i,j,k+1} - h_{31} f_{i,j,k+2}}{h_{31} h_{32} \left(h_{32} - h_{31}\right)}$$
(38)

First Regular Forward Derivatives

For equal grid spacings in each of the three coordinate directions, defined according to h., - h12/2 = h1

$$h_{21} = h_{22}/2 = h_2$$
 $h_{31} = h_{32}/2 = h_3$

Eqs. (36) - (38) reduce to
$$\frac{\partial f}{\partial J_{i}}\Big|_{i,j,k} = \frac{-3 f_{i,j,k} + f_{i+1,j,k} - f_{i+2,j,k}}{2h_{i}}$$
(40)

$$\frac{\partial f}{\partial d_{\bullet}}|_{i,j,k} = \frac{-3f_{i,j,k} + 4f_{i,j+1,k} - f_{i,j+2,k}}{2h_{\bullet}} \tag{41}$$

$$\frac{2f}{dk_3})_{i,j,k} = \frac{-3f_{i,j,k} + 4f_{i,j,k+1} - f_{i,j,k+2}}{2h_3}$$
 (42)

Second Irregular Forward Derivatives

Irregular Forward Derivatives

$$\frac{\partial^2 f}{\partial x^2}\Big|_{i,j,k} = 2\left[\frac{-h_{12}f_{i+1,j,k} + (h_{12}-h_{11})f_{i,j,k} + h_{11}f_{i+2,j,k}}{h_{11}h_{12}(h_{12}-h_{11})}\right] \qquad (42)$$

$$\frac{\partial^{2}f}{\partial k_{2}^{2}}\Big|_{i,j,k} = 2\left[\frac{-h_{22}f_{i,j+1,k} + (h_{22}-h_{21})f_{i,j,k} + h_{21}f_{i,j+2,k}}{h_{21}h_{22}(h_{22}-h_{21})}\right]$$
(44)

$$\frac{\partial^{2}f}{\partial d_{3}^{2}}\Big|_{i,j,k} = 2\left[\frac{-h_{32}f_{i,j,k+1} + (h_{32}-h_{51})f_{i,j,k} + h_{31}f_{i,j,k+2}}{h_{51}h_{32}(h_{32}-h_{31})}\right]$$
(45)

Second Regular Forward Derivatives

With equal grid spacings, according to Eq. (39), Eqs. (43) -

$$\frac{\partial^{2}f}{\partial d_{i}^{2}}\Big|_{i,j,k} = \frac{-2f_{i+1,j,k} + f_{i,j,k} + f_{i+2,j,k}}{h_{i}^{2}}$$
(46)

$$\frac{\partial^{2}f}{\partial d_{2}^{2}}\Big|_{i,j,k} = \frac{-2f_{i,j+1,k} + f_{i,j,k} + f_{i,j+2,k}}{h_{2}^{2}}$$
(47)

$$\frac{\partial^2 f}{\partial d_3} = \frac{-2fi,j,k+1 + fi,j,k + fi,j,k+2}{h_3^2}$$

First Irregular Backward Lierivatives

$$\frac{\partial f}{\partial \lambda_{2}}|_{ijj,2} = \frac{h_{23}f_{i,j-2}, k + (h_{24} - h_{23})f_{i,j,k} - h_{24}f_{i,j-1,k}}{h_{23}h_{24}(h_{24} - h_{23})}$$
(50)

$$\frac{\partial f}{\partial J_3}\Big|_{i,j;k} = \frac{h_{32}^2 f_{i,j,k-2} + (h_{34} - h_{33}) f_{i,j,k} - h_{34}^2 f_{i,j,k-1}}{h_{33} h_{34} (h_{34} - h_{33})}$$
(51)

First Regular Backward Derivatives (h, =:
$$\frac{h_{i4}}{2} = h_{i}$$
, etc.)

$$\frac{2f}{2d_{i}}\Big|_{i,j,k} = \frac{f_{i-2,j,k} + 3f_{i,j,k} - 4f_{i-1,j,k}}{2h_{i}}$$
(52)

$$\frac{\partial f}{\partial k_2})_{i,j,k} = \frac{f_{i,j-2,k} + 3f_{i,j,k} - 4f_{i,j-1,k}}{2h_2}$$
 (53)

$$\frac{\partial f}{\partial d_3}\Big|_{i,j,k} = \frac{f_{i,j,k-2} + 3f_{i,j,k} - 4f_{i,j,k-1}}{2h_3}$$
 (54)

Second Irregular Backward Derivatives $\frac{\partial f}{\partial h_i^2}\Big|_{i,j,k} = 2\left[\frac{h_{i3}f_{i-2,j,k} + (h_{i4} - h_{i3})f_{i,j,k} - h_{i4}f_{i-1,j,k}}{h_{i3}h_{i4}(h_{i4} - h_{i3})}\right] \tag{55}$

$$\frac{\partial^{2} f}{\partial u_{2}^{2}}\Big|_{i,j,k} = 2\left[\frac{h_{23} f_{i,j-2,k} + (h_{24} - h_{23}) f_{i,j,k} - h_{14} f_{i,j-1,k}}{h_{13} h_{24} (h_{24} - h_{23})}\right]$$
(56)

$$\frac{\partial^{2}f}{\partial d_{3}}\Big|_{i,j,k} = 2\left[\frac{h_{33}f_{i,j,k-2} + (h_{34} - h_{33})f_{i,j,k} - h_{34}f_{i,j,k-1}}{h_{33}h_{34}(h_{34} - h_{33})}\right]$$
 (57)

$$\frac{\partial f}{\partial k_i^2}\Big|_{ijk} = \frac{f_{i-2,j,k} + f_{i,j,k} - 2f_{i-1,j,k}}{h_i^2} \tag{58}$$

Second Regular Backward Derivatives

$$\frac{\partial f}{\partial k_{i}^{2}}\Big|_{i,j,k} = \frac{f_{i-2,j,k} + f_{i,j,k} - 2f_{i-1,j,k}}{h_{i}^{2}}$$
(59)

$$\frac{\partial f}{\partial k_{i}^{2}}\Big|_{i,j,k} = \frac{f_{i,j-e,\ell} + f_{i,j,k} - 2f_{i,j,i,k}}{h_{i}^{2}}$$
(59)

$$\frac{\partial^2 f}{\partial t_3^2}\Big|_{ij,k} = \frac{f_{i,j,k-2} + f_{i,j,k} - 2f_{i,j,k-1}}{h_3^2}$$
(60)

Mixed Derivatives

It can be shown from Eq. (23) That mixed derivatives require Values of the function at any six nodes in the vicinity of the point under consideration. Fig. 3 shows Various combinations of mixed dorivatives with respect to The coordinate axes of and dr. It is noted that the mixed central derivatives involve the four corner nodes as Well as Two adjacent modes in either of the two coordinate directions. The various combinations shown in Fig. 3 are summarized below for The coordinate directions &, and

Second Mixed Irregular Central Derivative With Respect to 2, and 22

a)
$$\frac{\partial^2 f}{\partial x_i \partial x_k} = \frac{1}{h_{2i} h_{2i} (h_{ii} + h_{i3}) (h_{2i} + h_{2i})} \left[h_{2i}^2 (f_{i+i,j+i,k} - f_{i-i,j+i,k}) - (h_{2i} - h_{2i}) (f_{i+i,j,k} - f_{i-i,j+i,k}) - (h_{2i} - h_{2i}) (f_{i+i,j,k} - f_{i-i,j-i,k}) \right]$$

$$- (h_{2i} - h_{2i}) (f_{i+i,j,k} - f_{i-i,j,k}) - h_{2i} (f_{i+i,j-i,k} - f_{i-i,j-i,k})$$

b)
$$\frac{\partial^2 f}{\partial \lambda_1 \partial \lambda_2} i_{i,j,k} = \frac{1}{h_{11} h_{13} (h_{11} + h_{13}) (h_{21} + h_{23})} \left[h_{13} (f_{i+1,j+1,k} - f_{i+1,j-1,k}) - (h_{13} - h_{11}^2) (f_{i,j+1,k} - f_{i,j-1,k}) - h_{11} (f_{i-1,j+1,k} - f_{i-1,j-1,k}) \right]$$

$$= (h_{13} - h_{11}^2) (f_{i,j+1,k} - f_{i,j-1,k}) - h_{11} (f_{i-1,j+1,k} - f_{i-1,j-1,k})$$

Eigit breguler N'ein 1800 on Mills Gerber 1800 Peringtives

Centra 1		4
Forward	$\begin{array}{c} c \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	
Backward	h 10	h ₁₁
Corner	g)	h,, d,2

Second Mixed Irregular Firward Derivative With Raspect to &, and &

$$\frac{\partial f}{\partial l_1 \partial k_2} \Big|_{i,j,k} = \frac{1}{h_{21} h_{23} (h_{11} - h_{12}) (h_{21} + h_{22})} \Big[h_{23} (f_{i+1}, j_{+1}, k - f_{i+1}, k - f_{i$$

$$d) \frac{\partial^{2}T}{\partial x_{i}\partial k_{2}}\Big|_{i,j,k} = \frac{1}{h_{11}h_{13}(h_{21}-h_{22})(h_{11}+h_{13})} \Big[h_{13}^{2}(f_{i+1,j+1,k}-f_{i,j+1,k}) - f_{i+1,j+2,k} + f_{i,j+2,k} - h_{11}^{2}(f_{i-1,j+1,k}-f_{i,j+1,k}) - h_{11}^{2}(f_{i-1,j+1,k}-f_{i,j+1,k}) - f_{i-1,j+2,k} + f_{i,j+2,k}\Big]$$

Second Mixed Irregular Backward Derivative With Respect to & and &z

$$\frac{\partial^{2}f}{\partial \lambda_{1}\partial \lambda_{2}} = \frac{-1}{h_{21}h_{23}(h_{13}-h_{14})(h_{21}+h_{23})} \left[h_{23}^{2}(f_{i-1},j+1,k-f_{i-2},j+1,k+f_{i-2$$

$$f) \frac{\partial^{2} f}{\partial \lambda_{i} \partial \lambda_{j}} = \frac{-1}{h_{11} h_{13} (h_{28} - h_{24}) (h_{11} + h_{13})} \left[h_{13}^{2} (f_{i+1}, j-1, k - f_{i+1}, j-2, k + f_{i,j-2}, k - f_{i,j-1, k}) - h_{24}^{2} (f_{i-1}, j-1, k - f_{i,j-1}, k - f_{i,j-2}, k + f_{i,j-2}, k) \right]$$

$$- f_{i-1}, j-2, k + f_{i,j-2}, k \right]$$

Second Mixed Irregular Corner Derivative With Respect to w, and of

$$\frac{\partial \hat{f}}{\partial k_{1}\partial k_{2}} = \frac{1}{h_{11} h_{12} h_{21} h_{22} - h_{21}} \left[h_{12} h_{22} - f_{13} \right] \left[h_{12} h_{22} \left(f_{13} \right)_{j=1, k} - f_{13} \right]$$

$$- f_{1,j+1, k} + f_{1,j, k} - h_{11} h_{23} \left(f_{13} \right)_{j+2, k} - f_{13} \right]$$

$$- f_{1,j+2, k} + f_{1,j, k} \right]$$

$$(67)$$

Second Mixed Regular Derivatives

All of the above results can be reduced to regular derivatives with respect to either di, do or both coordinates by making the substitutions

$$h_{\mu} = h_{13} = \frac{h_{12}}{2} = h_{1}$$
 (68)

$$h_{21} = h_{23} = \frac{h_{22}}{2} = \frac{h_{24}}{2} = h_{2}$$
 (69)

The various derivatives are summarised below for the case in which all grid spacings are equal (i.e., h, = h.).

Second Mixed Regular Central Derivative With Respect to & and h.

a), b)

$$\frac{\partial^{\frac{2}{4}}}{\partial d_{1}\partial d_{2}}\Big|_{i,j,k} = \frac{1}{4h^{2}} \Big(f_{i,j,j+1,k} - f_{i+1,j+1,k} - f_{i+1,j+1,k} + f_{i+1,j+1,k}\Big)$$
(71)

Second Mixed Regular Forward Derivative With Respect to &, and &_

$$\frac{-1}{2h^{2}}\left(f_{ij,j+1,k}-f_{i+2,j+1,k}-f_{i+1,j-1,k}+f_{i+2,j-1,k}\right) \tag{72}$$

$$\frac{3^{2}}{3^{1}d_{1}2d_{2}}\Big)_{i,j,k} = \frac{1}{2h^{2}}\left(f_{i-1,j+1,k} - f_{i-2,j+1,2k} - f_{i-1,j-1,k} + f_{i-2,j-1,k}\right)$$
 (74)

$$f) \frac{j^{2}}{2h^{2}} = \frac{1}{2h^{2}} \left(f_{i+1,j-1,k} - f_{i+1,j-2,k} - f_{i-1,j-1,k} + f_{i-1,j-2,k} \right)$$
 (75)

Second Mired Regular Corner Derivative With Respect to &, and de

SMHERICAL	COORDINATES

	2	/		2	į	3		4	:	చ		6	
0,	41	λ+2μ	0	λ	0	λ	0	C	6)	0	9	0	6)
1	3,	0	63	0	0	0	0	MIR	0	0	Ø	O	٤
2	re	0	(4)	C	0	0	9	C	0	0	0	14/(R xin q) @
,	51	2 \/R	0	2 (1+14)	RE	2 (2+14)/	RO	0	0	0	9		ري
•	Z	0	0	0	E	0	9	M	0	0	E	0	0
	3,	λ/R	0	(X+2/L)/	RE	λ/R	(4)	O	0	0	0	0	E)
	7,	0	(1)	0	ال	0	9	O	0	14 KR sin	9)		Ø
	5,	A wt	E Ø	Dust 9/A	20	(λ+2μ) cot	4/20	- M/R	0	0	Ø	0	Ø
2	7,	0	0	0	0	0	0	0	0	٥		μ	0
	3,	0	ال	0	0	0	0	Ö	G	M/R	9	0	Q
	8,	X KR sin	r P			(x+2 p) /RA		O	0	0	0	0	6
	5,	٥	0	0	Ü	0	0	O	9	- protq	R	- 11/R	Ø

TOROIDAL COORDINATES

~d1	λ+2μ	0	λ	0	λ	9	O	(J)	0		0	9
β_{l}	0	0	O	0	O	(9)	11/1		0	6	C	, 0
Y	O	9	O	0	0	0	0	0	0		M/(a+1	sin 45
: 82	7(a+2 r si	φ) (φ)	$\frac{\lambda+i\mu}{r}+\frac{\lambda}{a+}$	rom q	7 + (x+24)) 0	(e)	0	9	0	0
Z,	0	ပ	O	0	0	0	μ	(E)		9	{	E E
Ē,	7./24	Ð	(x+2m)/	4 9	λ/r	(2)	0	9	0	(2)	<u> </u>	0
7,	0	Ø	0	(D)	0	Θ	0	(E)	M/(a+rai	ng) (É	2)
8,	2+rsin	- q b	$\frac{\lambda \cos \varphi}{a + r \sin \varphi}$	- (Y)	(2+2 m) Con a+1 cm	\$ 3	- /4/1	O	0	O	c	> @
21	0	0	0	Θ	0	9	0	0	G	e	1	L O
B	O	0		9	0	9		0		0		,
7,	Ma+roi	14)	arra	(S)	2+1 mi	· Ø		9	1			> <i>\theta</i>
50	0	6	0	0	0	0	0	(i)	- 11 coo			in q G pir. P